

## Speed Adjustment for Brushless DC Motors Using Microcontrollers

Truong ThiQuynh Nhu<sup>1</sup>, Tran ThiHai Yen<sup>2</sup>

<sup>1</sup>Automation Department, Thai Nguyen University of Technology, Vietnam

<sup>1</sup>quynhnhu-tdh@tnut.edu.vn, <sup>2</sup>haiyentran86@gmail.com

**Abstract:** Brushless DC motors have many advantages so that they are widely used. Because there are no mechanical reversing parts using brush rings so this BLDC motor overcomes most of the disadvantages of common DC motors. Hence, in order to adjust the speed for this motor, we use microcontrollers to improve the quality of the system

**Keywords:** Brushless DC Motor, Microchip Dspic Microcontroller, Hall, Control, Speed Adjustment.

Symbols	Unit	Meaning
$R_a, R_b, R_c$	Om	Stator Phase Resistances
$V_a, V_b, V_c$	Voltage	Phase Voltages
$L_a, L_b, L_c$	H	Stator Phase Inductors
$i_a, i_b, i_c$	A	Stator Phase Currents
$M_{ab}, M_{ac}, M_{ba}, M_{bc}, M_{cb}, M_{ca}$	H	Mutual Inductance Among Phases
$e_a, e_b, e_c$	V	Electromotive Force of Phases a, b, c
$\omega_r$	Rad/s	Speed of Rotor
$T_e, T_L$	N.m	Electric Torque and Torque Load

### Abbreviations

BLDC BLDC-Brushless DC Motor

## I. INTRODUCTION

The brushless DC motor (BLDC) has no mechanical reversing parts using brush rings so this BLDC motor overcomes most of the disadvantages of common DC motors. This motor has high efficiency due to reduced power loss, no maintenance and small rotor inertia.

Automated systems using traditional electric motors are often designed with relatively inexpensive similar elements. The weaknesses of the similar systems are life expectancy of components and they are sensitive to changes in temperature. Another drawback of these systems is that it is difficult to expand and upgrade. Numerical control structures overcome all the disadvantages of the similar drive structures. High-speed digital signal processors allow the implementation of numerical control problems that require high resolution, high speed and large volume. In addition, they also allow the minimum delay time in the control loop. These high-performance controls also allow to reduce torque fluctuation and power loss. Continuous waveforms allow optimization of power elements and input filters.

In the article we use a Microchip Dspic microcontroller to adjust the speed of a brushless DC motor.

## II. THE SPEED-ADJUSTING EXPERIMENTAL SYSTEM FOR BLDC MOTORS

The connected blocks on the experimental table are like in Figure 1: The experimental object is a brushless DC motor. Speed response when changing the speed setting value from 30rad/s to 25rad/s after 3s and then changing again to 30rad/s, speed response when adjusting the regulator parameter. To adjust the speed we use the PSPIC33FJ64MC506 microcontroller to control the switching of valves of IGBT set. To determine the position of the rotor we use Hall sensors.

Fig.2 The experimental table of the control system: connected to the computer and results shown on the oscilloscope.

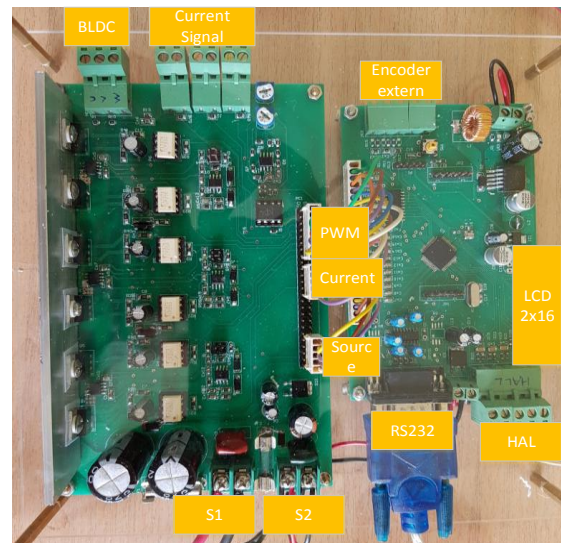


Fig.1. Connected Blocks on an Experimental Table

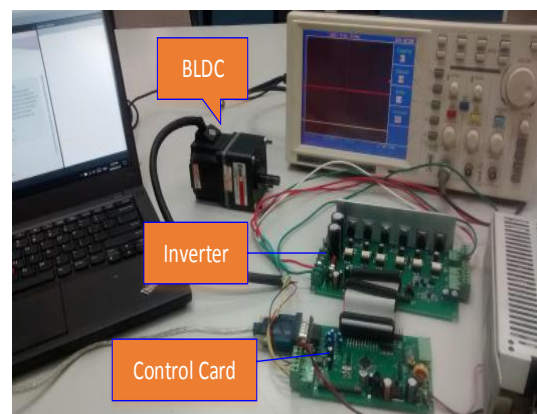


Fig. 2. The Experimental Table of BLDC Control System

### III. OVERVIEW OF A BRUSHLESS DC MOTOR, ALGORITHM MODEL AND METHOD OF BLDC MOTOR CONTROL

The structure of a brushless DC motor is very similar to a permanent stimulation synchronous AC motor with a permanent magnet. The basic difference of a brushless DC motor compared to a permanent stimulation synchronous AC motor is that it combines some means to determine the position of the rotor (or the position of the magnetic pole) to create electronic switch control signals. Therefore, the brushless DC motor is a combination of a permanent stimulation synchronous AC motor and an electronic reversing switch according to rotor positions. The position of the rotor is determined via position sensors. Most of the rotor position sensors (magnetic poles) are Hall elements, but there are also some motors using optical sensors.

Almost all brushless DC motors have Hall sensors hidden inside the stator, in the rear axle (auxiliary shaft) of the engine. Whenever the rotor's magnet poles pass through the area near the Hall sensors, the sensors send out high or low signals when the North or South pole go past the sensor. Based on the combination of signals from three Hall sensors, the exact switching order is determined.

In order for the BLDC motor to work, it is necessary to know the exact position of the rotor to control the process of switching off the semiconductor locks, powering the stator coils in a proper sequence. The torque is generated by the interaction of the magnetic field generated by the stator coils with the permanent magnet. To keep the motor rotating, the magnetic field produced by stator coils must rotate synchronously with the rotor's magnetic field at an angle  $\alpha$ .

*Algorithm Model and Control Method:*

#### 1. Algorithm Model of Brushless DC Motors:

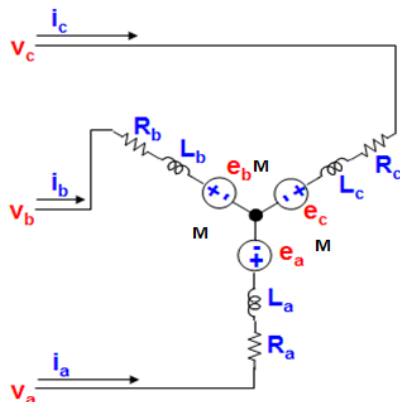


Fig. 3. Equivalent Circuit Diagram of BLDC

Voltage equation on coils:

$$v_a = R i_a + (L - M) \frac{d i_a}{d t} + e_a$$

$$v_b = R i_b + (L - M) \frac{d i_b}{d t} + e_b$$

$$v_c = R i_c + (L - M) \frac{d i_c}{d t} + e_c$$

$V_a, V_b, V_c$ : are phase voltages a, b and c.

$R_a = R_b = R_c = R$ : are stator resistors of phases a, b and c.

$L_a = L_b = L_c = L$ : are stator inductances of phases a, b and c.

$i_a, i_b, i_c$  are stator currents of phases a, b and c.

$M_{ab} = M_{ac} = M_{ba} = M_{bc} = M_{cb} = M_{ca} = M$  are the inductance between phases.

$e_a, e_b, e_c$  are the dynamic rates of phases a, b, c.

The electromagnetic torque of the motor is calculated through mechanical power and electrical power. Because the friction in the motor is mainly produced between the motor shaft and the bearing, this friction force is small. In addition, the engine fabrication material is also a type with high resistivity so it can be assumed that iron losses and copper losses are neglected. Therefore, the power input to the motor is also equal to the mechanical power on the axis end.

$$T_e = \frac{e_a i_a + e_b i_b + e_c i_c}{\omega_r}$$

Mechanical equation

$$T_e = B_m \omega_r + J_m \frac{d}{d t} \omega_r + T_L$$

$\omega_r$  is the mechanical speed of the rotor,  $T_e$  is the electromagnetic torque,  $T_L$  is the load torque and  $J_m$  is the inertial force.

#### 2. Control Method:

The control model for a contactless DC motor and how to implement it. Especially the simulation of PWM converter is done by switching functions.

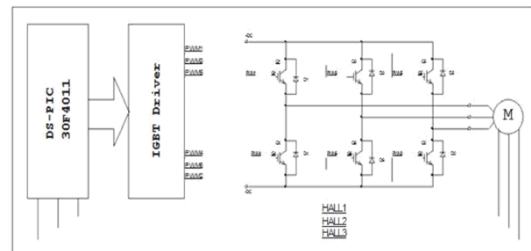


Fig. 4. Brushless DC Motor Control System

Figure 4 is the power circuit structure of the change system to control 3-phase BLDC motors.

To control the BLDC motor, we control the switching of the corresponding valves through pulse width modulation. The pulse width modulation is performed by Microprocessor: DSPI 33 FJ64MC506\_I / PT

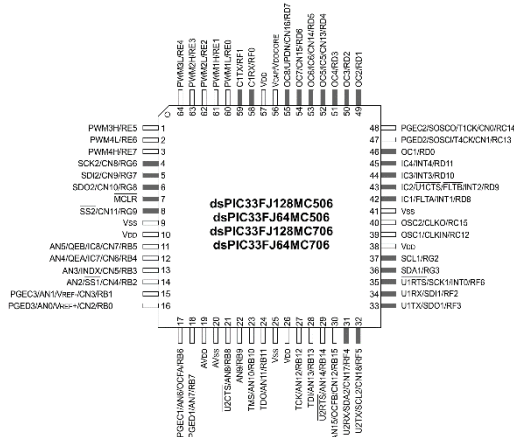


Fig. 5. Microcontroller Components DSPIC33FJ64MC506

Using DSPI microprocessor as the main controller, generating PWM pulses for buffers, the microcontroller must perform the task of getting the signals from the HALL sensors.

Modulation method of PWM: the control structure consists of 2 layers, the inner one is the current control loop, the outer one is the speed control loop:

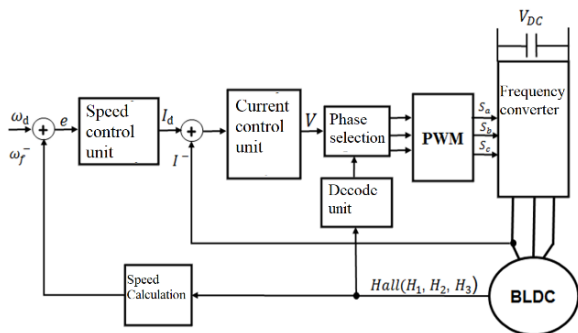


Fig. 6. The Proposed Controller Structure Diagram for BLDC

From that we have a single-phase replacement diagram:

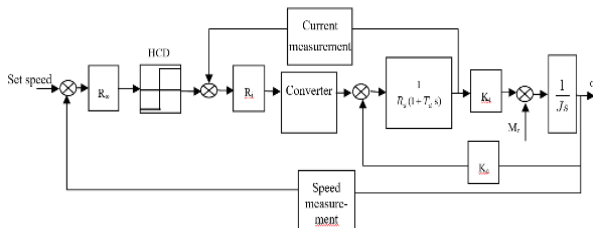


Fig. 7. The Converter is Represented by the Transfer Function:

$$W_{bd} = \frac{K_{bd}}{(1 + sT_{bd})} = \frac{4.8}{1 + 0.001s}$$

$$K_{bd} = \frac{U_{cd\max}}{U_{dk\max}} = \frac{24}{5}$$

Select  $T_{bd} = 0.001$

*Synthesis of Current Circuit Loop:*

Due to the high power motor, we can ignore the change of dynamic reaction E in a short time, so we can simplify the current control loop circuit as follows:

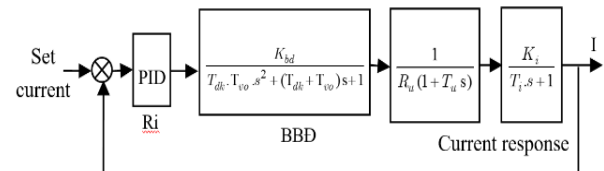


Fig. 8. The Minimal Current Loop Circuit Model of BLDC Motors

Applying the optimal standard of the module for the above object, we have the current regulator as PI block. The current regulator will look like this:

$$R_i = \frac{1 + T_s s}{K T_s s}$$

Inside: and  $T = T_u$

Replace the number we have:

$$R_i = \frac{1 + 0.03s}{0.01s}$$

*Synthesis of Speed Loop:*

When synthesizing the speed loop, the current loop is replaced by the standard function and ignoring the influence of dynamic reaction and torque of resistance because in a small time the components change slowly.

The time constant  $T_s$  is small, so we can ignore the component  $s^2$  in the denominator of the standard function to facilitate the synthesis. Then we have the model of speed loop circuit as follows:

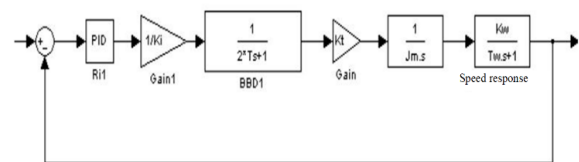


Fig. 9. Model of Speed Loop Circuit of Motors

$$W_{dt} = \frac{K_i K_\omega}{K_i (1 + 2sT_s)(1 + sT_\omega)(sJ_m)}$$

Applying the symmetrical optimal standard for the above object, the speed regulator is as follows:

$$R_\omega = \frac{T_c}{2KT_s} \cdot \frac{1 + 4T_s'}{4T_s s}$$

#### IV. SIMULATION RESULTS

The BLDC motor with the following parameters:

Prated = 60W;  $p = 4$ ;  $R_s = 2.08\Omega$ ;  $L = 5.5 \text{ mH}$ ;  $J = 0.00019 \text{ kg.m}^2$ ;

Simulating the layer control algorithms for brushless DC motors with feedback current DC-link.

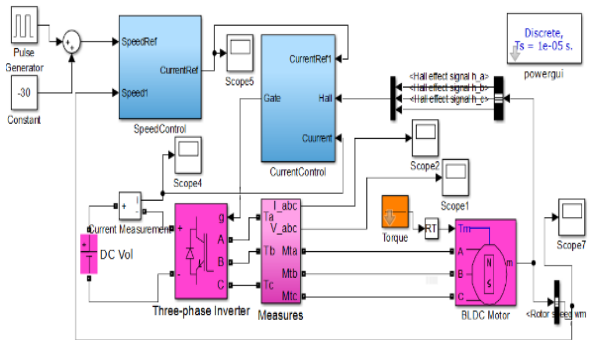


Fig. 10. Simulation Diagram Implemented on MATLAB - Simulink

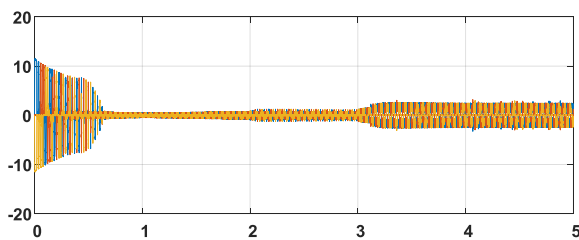


Fig. 11. Phase Currents of the BLDC Motor

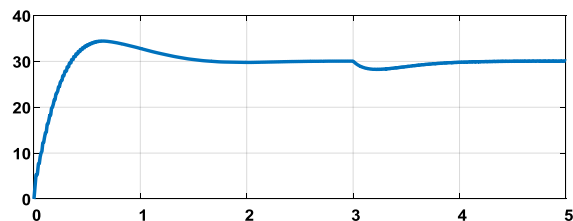


Fig. 12. Speed Response when Loading

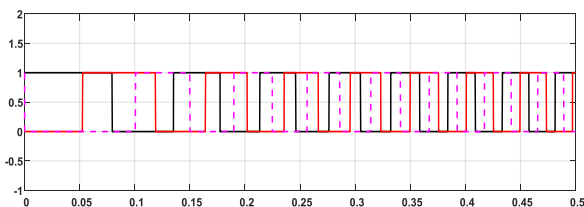


Fig. 13. Signal from Hall Sensors

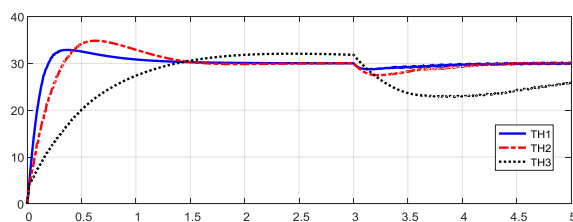


Fig. 14. Speed Response when Changing Parameters of the Regulator 1, 2, 3

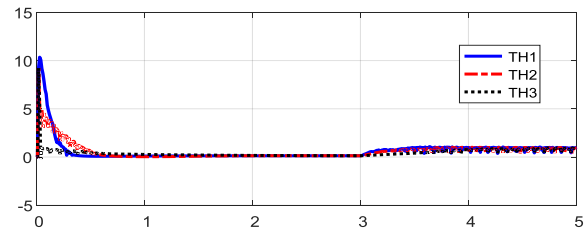


Fig. 15. Current Response when Changing Parameters of the Regulator 1, 2, 3

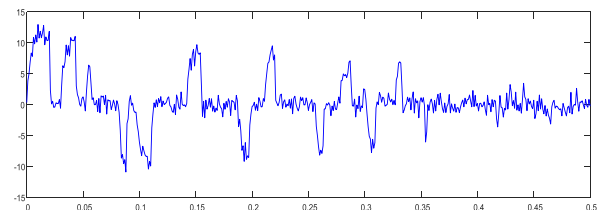


Fig. 16. The Form of Phase a Current when Experimenting

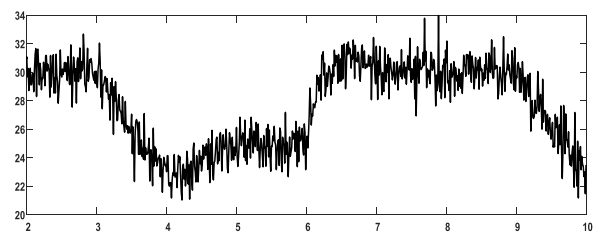


Fig. 17. Speed Response when Performing Experiments

From simulation results and experiments, we see that the proposed controller performs well the task of maintaining the set speed and stability under the condition of load disturbance.

#### V. CONCLUSION

When using the microcontroller to control the BLDC motor, the system has met the requirements. Besides, the layer control algorithm with the inner layer controlling the current, the outer layer controlling the speed also brings stable results, responding to different cases of the set values in both simulations and experiments.

#### VI. REFERENCES

- [1] M. R. Feyzi, M. Ebadpour, S. A. KH. Mozaffari Niapour, Arshya Feizi, and R. Mousavi Aghdam "A New Single Current Strategy for High-Performance Brushless DC Motor Drives" IEEE CCECE 2011 – 000420.
- [2] Ahmad Faiz Noor Azam, Auzani Jidin, Mohamed Azmi Said, Hatta Jopri, Mustafa Manap "High Performance Torque Control of BLDC Motor" 2013 International Conference on Electrical Machines and Systems, Oct. 26-29, 2013, Busan, Korea.

- [3] A. Purna Chandra Rao, Y. P. Obulesh and Ch. SaiBabu “Mathematical Modeling of BLDC Motor with Closed Loop Speed Control using PID Controller Under Various Loading Conditions” ARPN Journal of Engineering and Applied Sciences 2006-2012 Asian Research Publishing Network (ARPN).
- [4] IrajFaraji Davoudkhani, Mohsen Akbari “Adaptive Speed Control of Brushless DC (BLDC) Motor Based on Interval Type-2 Fuzzy Logic ” 2016 24th Iranian Conference on Electrical Engineering (ICEE).
- [5] Hemant Melkote, Member, IEEE, and Farshad Khorrami, Senior Member, IEEE “Nonlinear Adaptive Control of Direct-Drive Brushless DC Motors and Applications to Robotic Manipulators “ IEEE/ASME Transactions on Mechatronics, Vol. 4, No. 1, March 1999.
- [6] José Carlos Gamazo-Real, Ernesto Vázquez-Sánchez and Jaime Gómez-Gi “ Position and Speed Control of Brushless DC Motors Using Sensorless Techniques and Application Trends ”Sensors 2010, 10, 6901-6947; doi:10.3390/s100706901.
- [7] Adel A. El-samahy, Mohamed A. Shamseldin “Brushless DC motor tracking control using self-tuning fuzzy PID control and model reference adaptive control” Ain shams engineering Journal 2016.
- [8] Hans Butler, GerHonderd, and Job van Amerongen “Model Reference Adaptive Control of a Direct-Drive DC Motor ” IEEE Control Systems Magazine, 0’272-170818910100-0080 \$0100 0 1989 IEEE.
- [9] Yong Liu, Student Member, IEEE, Z. Q. Zhu, Senior Member, IEEE, and David Howe “Direct Torque Control of Brushless DC Drives With Reduced Torque Ripple” IEEE Transactions on Industry Applications, Vol. 41, No. 2, March/April 2005.
- [10] Salih Baris Ozturk Hamid A. Toliyat “Direct Torque Control of Brushless DC Motor with Non-sinusoidal Back-EMF” 1-4244-0743-5/07/ 2007 IEEE.